

Analysis of Lift and Drag Forces at Different Azimuth Angle of Innovative Vertical Axis Wind Turbine

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Abstract: Vertical Axis Wind Turbines development was ignored as compared to horizontal axis wind turbines, due to its inability to generate large power. VAWT's have the advantage of working in turbulent wind and at low height. The power generated by VAWT depends upon the drag and lift forces acting on the blades. This paper is focused on analysis of drag and lift forces at different tip speed ratio acting at different azimuth angle of wind turbine. Computational fluid dynamics analysis of turbine is done by using K ω Shear Stress Transportation turbulence model. Computation is done to calculate Drag coefficients, Lift coefficients, and pressure and velocity distribution on wind turbine. Coefficient of lift is maximum at 35° and minimum at 90°, drag coefficient is maximum at 60° and minimum at 150°, pressure is maximum at 30° and minimum at 90°.

Keywords: VAWT, CFD, Power Coefficient, Lift Force, Drag Force, Azimuth Angle

1. Introduction

VAWT has its pros and cons as compared to HAWT. VAWT do not require pitch and yawing, they can harness wind power coming from any direction. The gear box are installed on ground, due to which maintenance is easier. VAWT can be used at lower heights where the wind is turbulent which increases its utility in urban stand-alone power generation. However, its one of the drawback is high torque fluctuations with each revolution of blades. VAWT blades face inconsistent angle of attack through 360° rotation. The lift and drag forces vary as the angle of attack varies. A detailed study should be done of the lift and drag forces generated

Earlier attempts were made to study the airfoil characteristics over 180° and 360° angle of attack, detailed aerodynamic flow around wind turbines airfoils has been carried in the region immediately before and after stall [1,2]. Similar work on aerodynamic complexities of VAWT has been done using PIV techniques [3].

Attempts were made to improve the self-starting speed of Darrius hydrokinetic wind turbine by studying the forces acting on the straight blades and varying the pitch angle [4]. Novel vertical axis sail rotor was used and force analysis for one complete rotation was made for enhancement of

self-starting speed [5]. Effect of Cambered airfoil on self-starting speed of vertical axis wind turbine was studied and found that cambered airfoil improves the self-starting speed with low power coefficient as compared to symmetrical blades [6,7].

Performance analysis of wind turbine was conducted numerically by using CFD, where the focal point of research was to study aerodynamics, to harness maximum power at low wind speed, effect of design parameters, orientations on the performance of wind turbine [8, 9] attempts were made in past to analyze the flow structure visualization of the airfoil NACA 4518 of H rotor Darrius VAWT at different angle of attack and speed. This research provided preliminary information for complex unsteady analysis of VAWT [10]. Reviewed the development of CFD as applied by the wind energy community from small scale to large scale from the flow around 2D airfoil to the flow through entire wind farm [11]. Flow field condition, wake evolution, separation of flow for Savonius Vertical Axis Wind Turbine was studied. It was understood that decrease in aspect ratio, 3 D CFD model will be required to get accurate predictions. Authors observed that there is variation of flow angle with respect to blades, strong unsteady effects including separation and vortex shedding. K ϵ model was used to obtain good result. CFD analysis was carried out to study the behavior of Savonius wind turbine under flow

field condition and to determine the performance and evolution of wake geometry. Analysis of lift and drag forces in a wind turbine blade and the effect of angle of attack on the efficiency of wind turbine blade [12]. Efforts were made to investigate effect of lift and drag forces on the performance of the VAWT. NACA 4420 airfoil blade was taken for analysis, lift and drag forces were measured at different sections of blade at different angle [13]. Numerical analysis was carried out on two and three dimensional unsteady computational fluid dynamic models to understand the aerodynamics of the performance. It was observed that below Re 30000 the performance of the turbine is degraded by a smooth rotor finish but above it the turbine performance is upgraded. Researchers have also studied the effect of solidity on the power coefficients. The blade rotor gives better performance as compared to two blade rotor. It was revealed that the performance coefficient predicted by the two dimensional computational model is significantly greater than that of the experimental and three dimensional CFD models [14]. Simulated the two dimensional unsteady flow field of the vertical axis wind turbine numerically for different turbulence models. Researchers found that at the constant speed of the wind and rotation, the total torque of the vertical axis wind turbine would change periodically [15].

In this paper an innovative turbine were modelled in ANSYS. Computational Fluid dynamics (Fluent) with $K-\omega$ Shear Stress Transportation turbulence model has been used to simulate the lift and drag forces at different tip speed ratio and azimuth angle. Analysis of total lift and drag forces is made and its effect has been studied.

2. Numerical Analysis

ANSYS FLUENT has been used for complete analysis of wind turbine. Conservation of momentum in an inertial (non-accelerating) reference frame is described by

$$\frac{\partial \rho}{\partial t} (\rho \vec{v}) + \nabla \cdot (\rho \vec{v} \vec{v}) = -\nabla p + \nabla \cdot (\vec{\tau}) + \rho \vec{g} + \vec{F} \quad (1)$$

The equation for conservation of mass, or continuity equation, can be written as follows:

$$-\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{v}) = S_m \quad (2)$$

ANSYS Fluent has been used for complete analysis of wind turbine. Using CFD simulation lift force, drag force and pressure on the turbine rotor is predicted. The 3 D geometry of Vertical Axis Wind Turbine has been created by using pre-processor Design Modular. Dimensions of the wind turbine are governed by wind tunnel test section size in which the experimentation is to be carried out. Turbine rotor diameter is 200 mm .NACA 68-613 cambered airfoil has been used in innovative VAWT. Cambered airfoil has the advantage of self-starting at low wind speed. Two blades placed orthogonal to each other with leading and trailing edge placed opposite to each other. Three flaps placed centrally between the two blades as shown in Figure.1.Flaps are made of 'S' shape so as

to having concave and convex geometry. The height of blades and flaps are 210 mm.

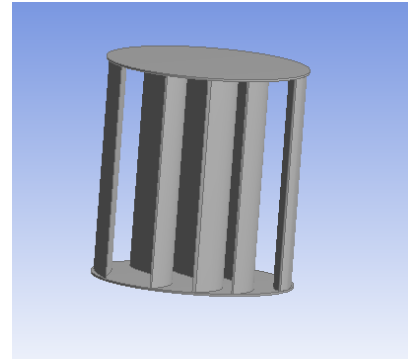


Figure 1. Geometry of three story VAWT.

To perform the dynamic simulation, Moving Reference Frame (MRF) capability of CFD solver has been used which allows to model problems involving moving parts. The Moving reference frame is activated in selected zone, that modifies the equation of motion with additional acceleration terms which occurs due to transformation from stationary to Moving Reference Frame. By solving the equations in steady state manner, the flow around the moving part is modeled. The moving reference frame does not account for the relative motion of a moving zone with respect to adjacent zones. Thus the mesh remains fixed for computation. The turbine is enclosed in MRF coaxially. The MRF is enclosed in a computational flow domain. The flow domain is having cylindrical shape. It was extended in axial direction about 4 diameters upstream and 8 diameters downstream of the rotor. This was to make sure that air fully extended. The fluid flow domain diameter is twice the diameter of the rotor. The left side of the domain is named as velocity inlet. The blockage ratio is kept minimum to bring the simulation close to field testing.

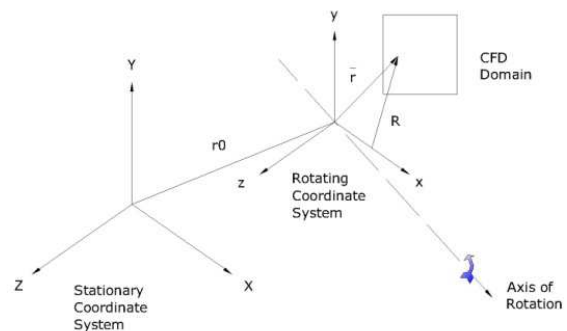


Figure 2. MRF principle.

Meshing is unstructured with growth rate of 1.5. The skewness is 0.289 and the aspect ratio is 1.8. The total number of nodes is 1, 72,895. All the computations were done in ANSYS FLUENT. The solver used was Pressure based, absolute velocity with steady time. $K-\omega$ SST turbulence model with standard wall function is used. Cell zones created are

turbine, MRF and Computational flow domain. Inlet velocity is varied in the range of 9- 11 m/sec. The pressure at the outlet is kept 0 Pascal. The turbine and MRF wall is considered as moving wall with rotational velocity along Z axis with no slip.

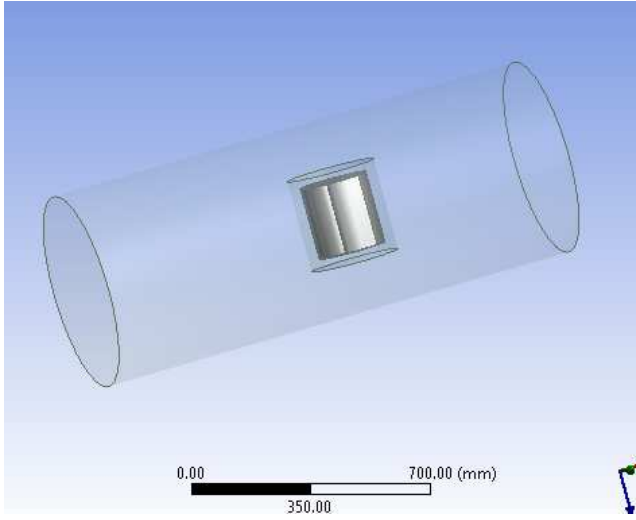


Figure 3. Turbine model placed in Moving Reference Frame and Stationary Computational Domain.

3. Result and Discussion

Vertical axis wind turbine model having two blades and three flaps has been simulated for tip speed ratio range from 2.0-2.55. The rotational speed range of rotor is taken 900-1100 rpm. Lift force and drag force were noted for different azimuth angle ranging from 0-180°. Maximum pressure, pressure and velocity distribution was also studied.

3.1. Tip Speed Ratio (TSR)

The TSR is calculated as the ratio between peripheral velocity and upstream wind velocity:

$$TSR = \frac{U}{V_w} \quad \text{Eq (3)}$$

3.2. Lift Force and Drag Force

The forces driving Vertical Axis Wind Turbine can be described in more detail with the help of Figure 5. There are two important velocity components. There is the velocity of the airfoil relative to the shaft, which is at all times parallel to the chord, having a magnitude equal to the rotational speed multiplied by the radius. There is also the velocity of the wind, which is approximated as a constant velocity in one direction. The resultant of these two velocities is the velocity of the air relative to the airfoil. The angle between this resultant velocity and the chord of the airfoil is called the angle of attack (α).

Lift is created by a pressure differential, which occurs whenever there is an angle of attack, α , not equal to zero. In the 0° azimuth position and the 180° position, $\alpha = 0^\circ$. At this point, only a drag force exists. Lift begins to be created as the blades rotate out of these two positions and α increase [7].

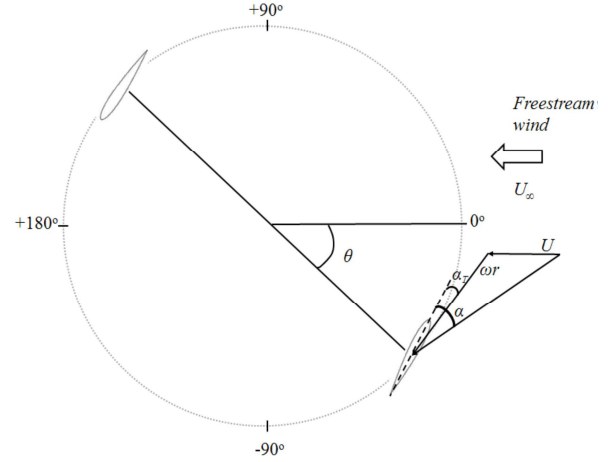


Figure 5. Lift and drag forces acting on blade at different azimuth angle.

The lift and drag forces are found numerically. Coefficient of lift and drag are calculated by Eq(4) and Eq(5).

$$F_D = \frac{1}{2} \rho A V^2 C_D \quad (4)$$

$$F_L = \frac{1}{2} \rho A V^2 C_L \quad (5)$$

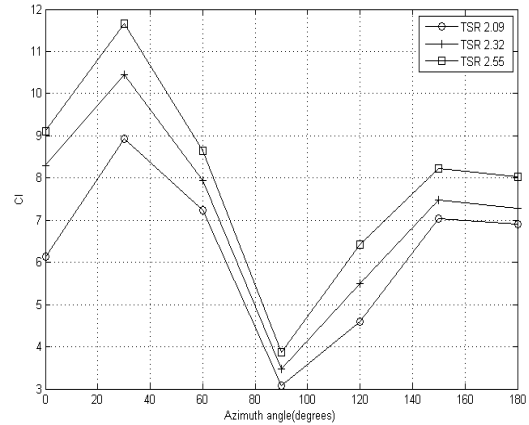


Figure 6. Lift coefficient vs Azimuth angle.

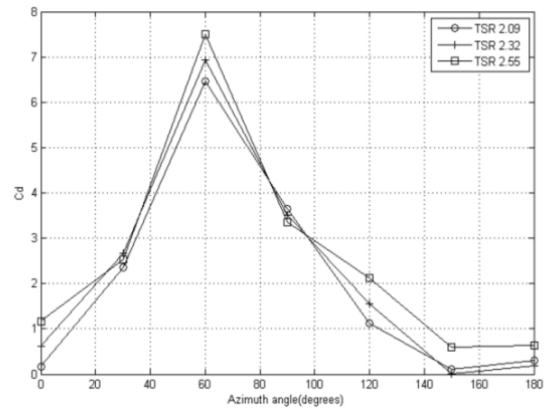


Figure 7. Drag coefficient vs Azimuth angle.

Figure 6 shows lift behaviour of lift force with respect to

azimuth angle at different tip speed ratio. It is seen that lift force is maximum at 30° and then further reduces to minimum at 90° and then starts increasing gradually from 90° and reaches next peak to 150° for the rotation of rotor from $0-180^\circ$. At 0° the lift force component is parallel to the wind flow where no tangential force is exerted on the blade. As the blade rotates from $0-90^\circ$ the lift force acting on the blade goes on increasing which in turn exerts tangential force on the blade. As the blades are fixed, their movement is constrained, that makes the turbine to rotate. As the blade progresses from $90-180^\circ$, it is covered by flaps due to which the blade is not exposed to wind. In this turbine two blades are used one of the blade is exposed to wind which contribute to lift and generation of tangential force. From figure 7, it is found that drag force is maximum at 60° and then reduces to minimum at 150° . The drag force on the turbine is because of the wind force acting on the concave and convex shape of the flaps. As the drag coefficient for concave surface is more than that of convex shape which dominate and rotates the turbine.

3.3. Static Pressure and Velocity Contours

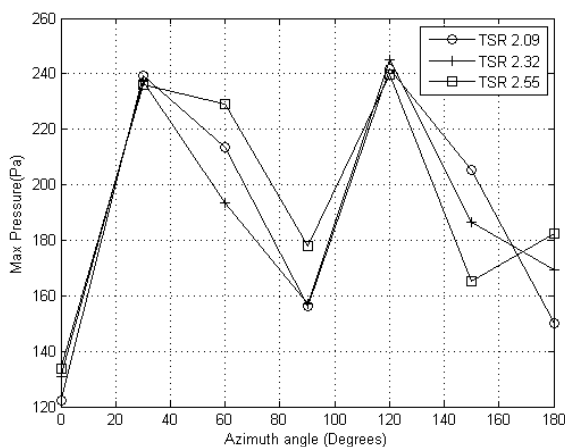
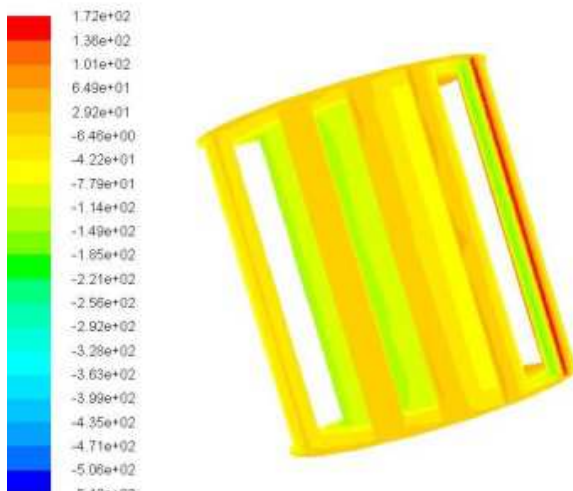
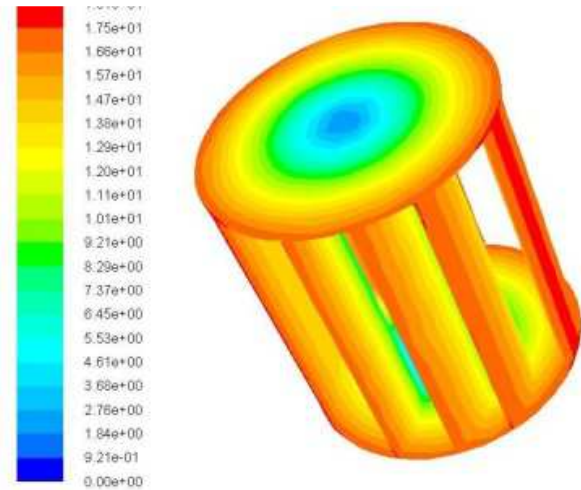


Figure 8. Max Pressure vs Azimuth angle.



(a)



(b)

Figure 9. Static Pressure and velocity contours.

From figure 8, it reveals that pressure magnitude escalates from $0-30^\circ$ and then further diminishes to minimum at 90° , reoccurrence of peak at 120° is seen again reducing to 150° . Figure 9 (a) shows static pressure plots. Pressure on the up stream side of the turbine is maximum as compared to the down stream side of the turbine. this pressure difference between upstream side and down stream side causes lift force in the turbine which makes it to rotate. Figure 9(b) shows velocity contour, in which it is seen that velocity aggravates from centre to its periphery.

4. Conclusion

A innovative vertical axis wind turbine has been modelled in design modeler of ANSYS and computational fluid dynamics analysis has been done in fluent. K ω Shear Stress Transportation turbulence model has been used. An attempt has been made to design the turbine in the view of harnessing maximum power in the wind. The coefficient of power developed by the turbine depends upon lift force, drag force and pressure acting on the turbine blades and flaps at different azimuth positions at different tip speed ratio. Lift force is maximum at 30° and then further reduces to minimum at 90° and then starts increasing gradually from 90° and reaches next peak to 150° for the rotation of rotor from $0-180^\circ$. At 0° the lift force component is parallel to the wind flow where no tangential force is exerted on the blade. As the blade rotates from $0-90^\circ$ the lift force acting on the blade goes on increasing which in turn exerts tangential force on the blade.

It is found that drag force is maximum at 60° and then reduces to minimum at 150° . The drag force on the turbine is because of the wind force acting on the concave and convex shape of the flaps. As the drag coefficient for concave surface is more than that of convex shape which dominate and rotates the turbine. Pressure magnitude rises from $0-30^\circ$ and then further diminishes to minimum at 90° , reoccurrence of peak at 120° is seen again reduces to 150° . Pressure on the up stream side of the turbine is maximum as compared to the down

stream side of the turbine. This pressure difference between upstream side and down stream side causes lift force in the turbine which makes it to rotate. Velocity aggravates from centre to its periphery of the turbine.

5. Nomenclature

A: Swept Area
 F_D : Drag force
 F_L : Lift force
 v : Wind velocity
 C_D : Coefficient of drag
 C_L : Coefficient of lift
 S_m : Mass source
 \vec{F} : Force vector
 U : Rotor speed
 ρ : Density
 $\bar{\tau}$: Stress tensor

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